



Hydrophone Sensor Integrated with APL Snake Robot

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- Integrate one or more optical hydrophones into the current APL snake robot manipulator to allow accurate ultrasound readings of tip position.
- Obvelop software framework to allow communication between ultrasound machine, EM tracker, robot control system, and optical hydrophone.
- Visualize position data in useful and visually pleasing way (similar to Robodoc)
- Oevelop general purpose calibration methods

Motivation



Kutzer et al.

Current method

- Inaccurate
- Limited mobility
- Insufficient

Improvements

- Direct measurement
- Accuracy (≤ 1.3 mm)
- Improved visualization

Implementation plan

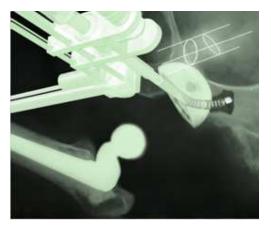
- Optical hydrophone in end-manipulator
- Measure ultrasound at tip
- Calculate US time of flight
- Multilateration from multiple sources
- Display data back to operator



Courtesy of Emad Boctor

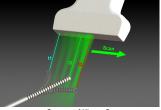
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Use case scenario





Courtesy of Xiaoyu Guo



Courtesy of Xiaoyu Guo

Kutzer et al.

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Use case scenario



Kutzer et al.

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Deliverables

Minimum

- Software and circuitry to measure time of flight
- Able to determine manipulator position within 5 mm

Expected

- Software and circuitry to measure time of flight
- Ø Able to determine manipulator position within 1 mm
- 8 Rudimentary visualization, shows position

Maximum

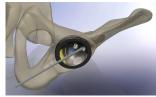
- Software and circuitry to measure time of flight
- Able to determine manipulator position within 1 mm
- 3 Able to determine manipulator orientation within 5 degrees
- Clean visualization, shows progress, material to remove

Previous concerns

- Hydrophone fibre curvature
 - Results unaffected down to 2cm radius
 - Noticeable attenuation at 1cm, but fibre unharmed
- 2 Lensing anatomy
 - Can use prior CT scan data to estimate refraction
- Oltrasound penetration
 - \approx 85% reflection at tissue-bone interface
 - $\approx 2\%$ penetration
 - But, only need binary signal, noise may be issue
 - Still need to test with real bone



Liu et al.

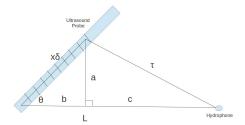


Liu et al.

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Calibration for element spacing



$$\tau^{2} = a^{2} + c^{2} \qquad \tau^{2} = a^{2} + c^{2}$$

$$L = b + c \qquad = (x\delta\sin\theta)^{2} + (L - b)^{2}$$

$$a = x\delta\sin\theta \qquad = L^{2} - 2Lx\delta\cos\theta + x^{2}\delta^{2}\cos\theta^{2}$$

 $b = x\delta\cos\theta$

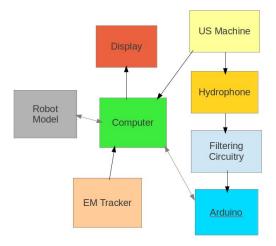
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$$\tau^2 = L^2 - 2Lx\delta\cos\theta + x^2\delta^2$$

- Perform non-linear least squares on 128 elements of array.
- Treat τ^2 as y, L, δ , and θ as parameters to solve for to minimize residuals.
- Used simulation and Gauss-Newton method to test, worked well for measurement errors below 5%, more complex techniques required to make it more robust.

- Use parameters from previous slide for two probe positions
- If position and orientation of probe known for both samples, can use the L and θ for each to determine the position of US array in frame of the US probe
- Possible to do with US imaging and fiducial, but wanted to find another method to simplify process

Workflow



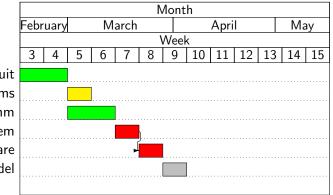
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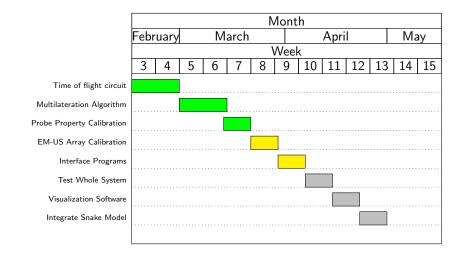
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Time of flight circuit Interface Programs Triangulation Algorithm Test Whole System Visualization Software Integrate Snake Model



New Schedule



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Deliverables

Minimum

- Software and circuitry to measure time of flight
- a Able to determine manipulator position within 5 mm

Expected (additional)

- **1** Able to determine manipulator position within 1 mm
- Q Rudimentary visualization, shows position
- **③** General purpose calibration methods

Maximum (additional)

- Able to determine manipulator orientation within 10 degrees
 - 2 Clean visualization, shows progress, material to remove

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Questions?

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