

Seminar Presentation

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Tool Gravity Compensation for the Galen Microsurgical System

The objective of this project is to:

- Develop models of tool gravity in static and dynamic modes
- Integrate the model into the control loop of the Galen robot to compensate for tool's gravity and dynamics
- Identify the deflection model of the Galen's arm in the presence of the operator's hand force

Paper selection

- *Learning optimal variable admittance control for rotational motion in human-robot co-manipulation.*
 - Dimeas, Fotios & Aspragathos, Nikos. (2015). Learning optimal variable admittance control for rotational motion in human-robot co-manipulation. IFAC-PapersOnLine. 48. 10.1016/j.ifacol.2015.12.021.

Why:

- Tool gravity compensation
- Variable admittance control

Summary of problem & key result

Problem

- Virtual damping, a key component in admittance control
 - Low damping → less resistance, fine positioning is reduced
 - High damping → fine positioning is increased, more resistance
- Variable damping can improve performance of the cooperative control framework
- Goal: Implement variable admittance control with a systematic approach

Summary of problem & key result

Key Results

- Implemented variable admittance control using a Fuzzy Model Reference Learning Controller (FMRLC)
- Allowed users to cooperate with a robot in a simple rotation task with significantly less energy exertion, in less time, and with less overshoot

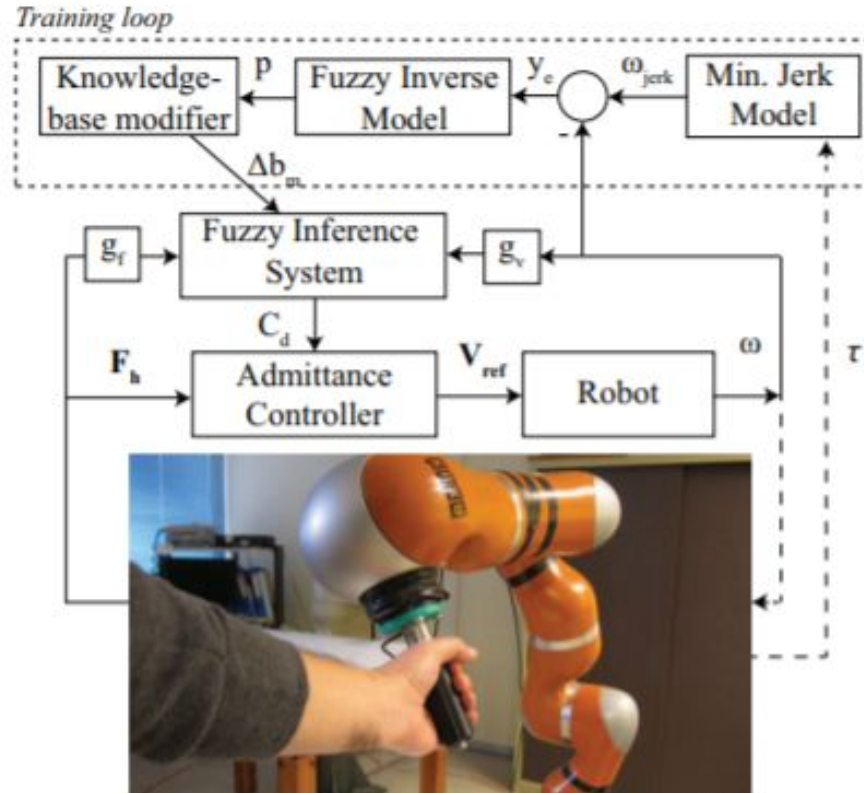
Significance of key result

- Presents a systematic approach to tune variable admittance control
 - Much of the prior literature tunes parameters using trial and error
- Presents an approach to regulate variable admittance control for rotation tasks
 - Most literature approaches variable admittance control for pure translation tasks

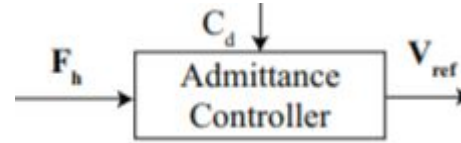
Necessary background

- Prior work by these authors for pure translation variable admittance control
 - Dimeas, F. and Aspragathos, N. (2014). Fuzzy Learning Variable Admittance Control for Human-Robot Cooperation. In IEEE International Conference on Intelligent Robots and Systems, 4770–4775. September 13-18, Chicago, IL, USA.
- Mathematics behind the minimum jerk trajectory model
 - Flash, T. and Hogan, N. (1985). The coordination of arm movements: an experimentally confirmed mathematical model. *The Journal of Neuroscience*, 5(7), 1688–1703.
- Knowledge of fuzzy control and FMRLCs
 - Passino, K.M. and Yurkovich, S. (1997). *Fuzzy Control*. Addison Wesley Publishing Company, California.

Technical Approach



Admittance Controller



- Goal: Impose desired velocities on end effector as a function of applied force

$$\mathbf{M}_d \dot{\mathbf{V}}_{\text{ref}} + \mathbf{C}_d \mathbf{V}_{\text{ref}} = \mathbf{F}_h$$

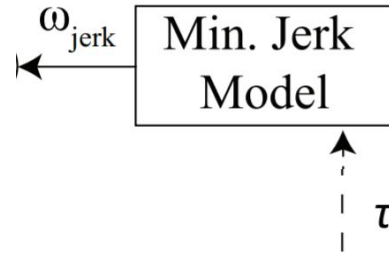
- \mathbf{F}_h = input forces / torques
- \mathbf{V}_{ref} = output velocities
- \mathbf{q}'_{ref} = joint velocities
- \mathbf{M}_d = virtual inertia
- \mathbf{C}_d = virtual damping/viscosity

$$\mathbf{V}_{\text{ref}} = \begin{bmatrix} \dot{\mathbf{p}}_r \\ \boldsymbol{\omega}_r \end{bmatrix} \in \mathbb{R}^3, \text{ translational velocities}$$

$$\mathbf{F}_h = \begin{bmatrix} \mathbf{f}_h \\ \boldsymbol{\tau}_h \end{bmatrix} \in \mathbb{R}^3, \text{ forces}$$
$$\in \mathbb{R}^3, \text{ torques}$$

$$\dot{\mathbf{q}}_{\text{ref}} = \mathbf{J}^{-1}(\mathbf{q}) \mathbf{V}_{\text{ref}}$$

Minimum Jerk Model



- During rotations, the trajectory followed by the human hand has minimal change in angular acceleration, and can be described by θ_{jerk}

$$\theta_{jerk}(\hat{t}) = \theta_0 + (\theta_f - \theta_0)(6\hat{t}^5 - 15\hat{t}^4 + 10\hat{t}^3)$$

$$\omega_{jerk}(\hat{t}) = \theta_f(30\hat{t}^4 - 60\hat{t}^3 + 30\hat{t}^2)$$

- t_f is the duration of the motion, $\hat{t} = t/t_f$, $\theta_0 = 0$ is the initial angle, and θ_f is the final angle.

$$y_e = \omega_{jerk} - \omega$$

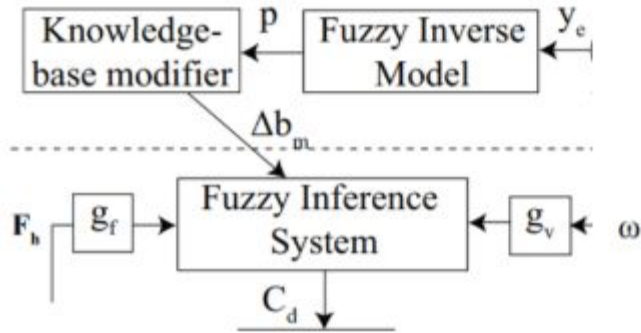
Fuzzy Model Reference Learning Controller

Initial Fuzzy Inference System rule-base:

C_d : 1 to 5 (low to high)

F_h & ω : -2 to 2 (neg high to pos high)

Triangular shaped membership functions



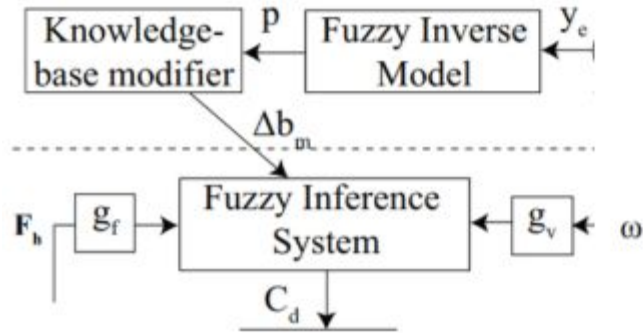
F_h = input forces / torques

ω = angular velocity

C_d = virtual damping

		C_d	F_h				
			-2	-1	0	1	2
ω	-2	1	2	3	5	5	
	-1	2	3	4	5	5	
	0	3	4	5	4	3	
	1	5	5	4	3	2	
	2	5	5	3	2	1	

Fuzzy Model Reference Learning Controller



Fuzzy Inverse Model rule-base:

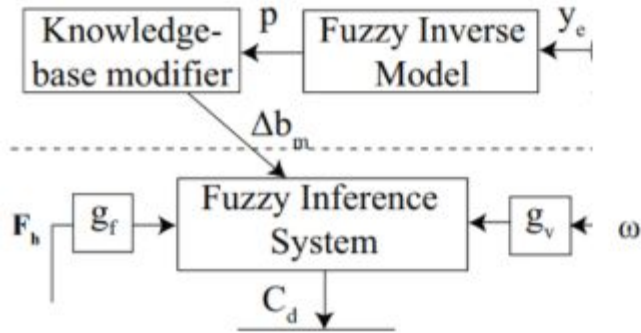
IF y_e is zero THEN p is zero.

IF y_e is positive THEN p is negative.

IF y_e is negative THEN p is positive.

$$y_e = \omega_{jerk} - \omega$$

Fuzzy Model Reference Learning Controller

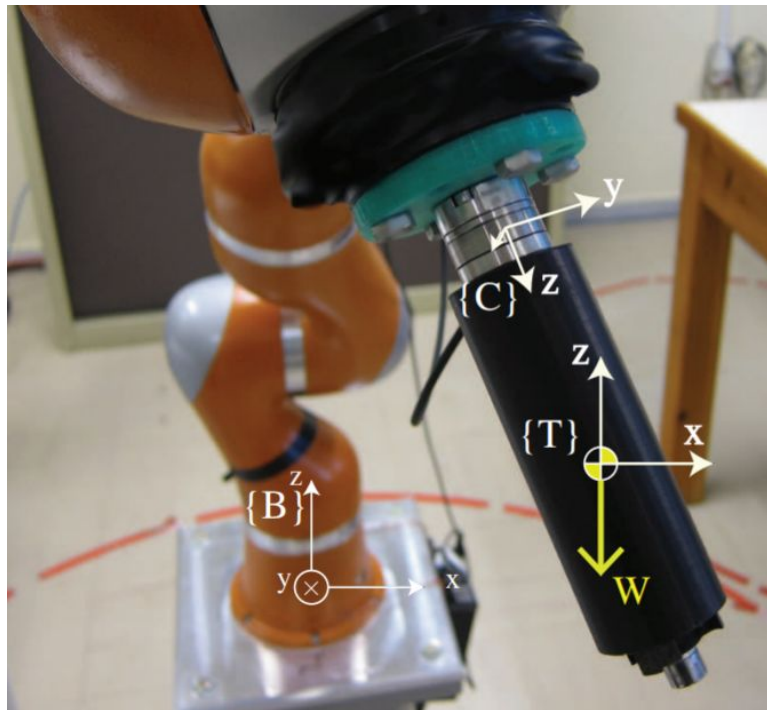


Knowledge-base modifier:

$$\Delta b_m(kT) = p\mu_m(\tau_h(kT - T), \omega(kT - T))$$

- The functions μ_m describes the certainty that a rule applies
- The function Δb_m describes how much to shift the output membership function

Tool weight compensation



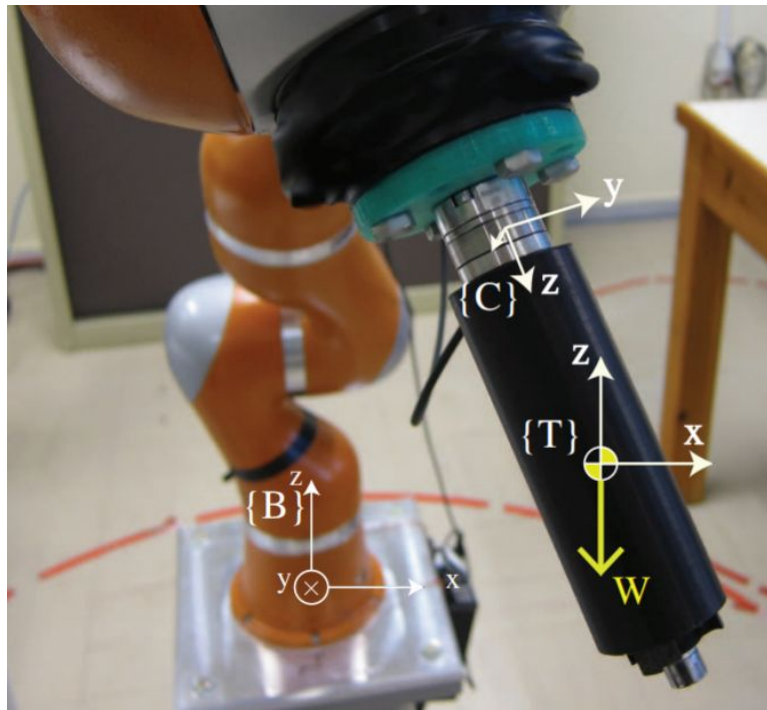
Transform forces and torques in tool frame to force sensor frame:

$$\mathbf{W} = \begin{bmatrix} \mathbf{f}_W \\ \boldsymbol{\tau}_W \end{bmatrix} \in \mathbb{R}^3, \text{ forces}$$
$$\boldsymbol{\tau}_W \in \mathbb{R}^3, \text{ torques}$$

$$\mathbf{f}_W = [0 \ 0 \ -m_t g]^T \quad \boldsymbol{\tau}_W = [0 \ 0 \ 0]^T$$

$$\begin{bmatrix} \mathbf{f}_W^C \\ \boldsymbol{\tau}_W^C \end{bmatrix} = \begin{bmatrix} \mathbf{R}_{CT} & 0 \\ -\mathbf{R}_{CT} \hat{\mathbf{p}}_T & \mathbf{R}_{CT} \end{bmatrix} \begin{bmatrix} \mathbf{f}_W^T \\ \boldsymbol{\tau}_W^T \end{bmatrix}$$

Tool weight compensation



Removing rebiasing weight and tool weight from force sensor readings

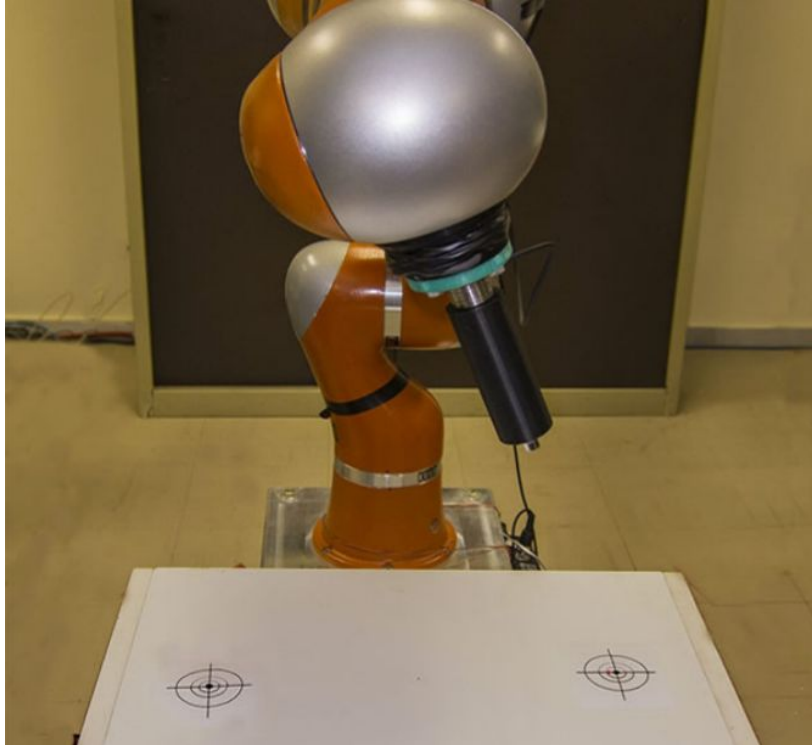
$$\mathbf{F}_{ext} = \mathbf{F}_{tot} - \mathbf{F}_{tot}^{init}$$

$$\mathbf{F}_{tot}^{init} = \mathbf{F}_{uncal} + \begin{bmatrix} \mathbf{f}_{W,init}^C \\ \boldsymbol{\tau}_{W,init}^C \end{bmatrix}$$

$$\mathbf{F}_{tot} = \mathbf{F}_h + \mathbf{F}_{uncal} + \begin{bmatrix} \mathbf{f}_W^C \\ \boldsymbol{\tau}_W^C \end{bmatrix}$$

$$\mathbf{F}_h = \mathbf{F}_{ext} - \begin{bmatrix} \mathbf{f}_W^C \\ \boldsymbol{\tau}_W^C \end{bmatrix} + \begin{bmatrix} \mathbf{f}_{W,init}^C \\ \boldsymbol{\tau}_{W,init}^C \end{bmatrix}$$

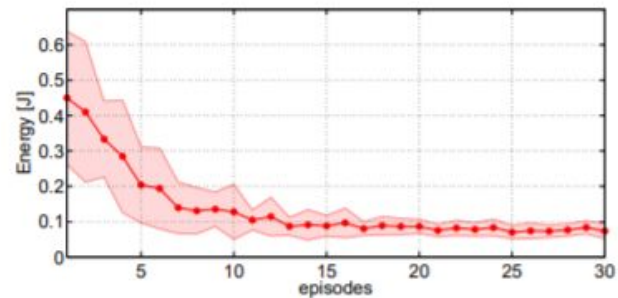
Experimental Evaluation



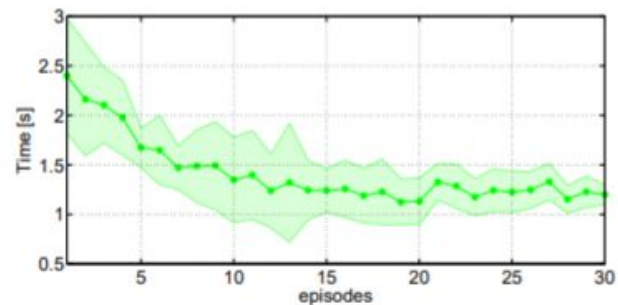
- A user study involving 7 participants
- Each subject rotated the KUKA LWR robot about the x-axis of frame {C}
 - Laser on end effector which points to goal regions, instructing subjects
 - Two sets of 30 transitions were recorded for each subject
- Output membership functions are initialized evenly distributed between 0 and 10 Nms/rad
- Output membership functions are updated throughout

Experimental Results

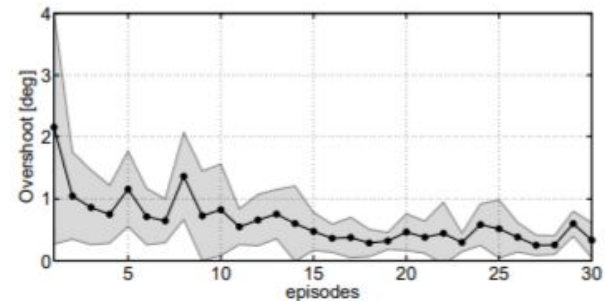
- The FMRLC significantly reduced energy exertion, time taken, and overshoot
- It converged to steady values after 10 episodes
- Thus, the FMRLC is more effective and systematic than manually tuned FISs for variable admittance control



(b)



(c)



(d)

Assessment

- Importance
 - Provides systematic approach to tune parameters for variable admittance control
 - Has potential in optimising human-robot cooperation in many settings
- Relevance
 - Provides a solid mathematical background for static gravity compensation and gives insight about adaptive adjustment of admittance gain

Assessment

- Good and Bad Points

Good	Bad
<ul style="list-style-type: none">● Clear justification of FMRLC approach● Explicit and helpful mathematics● Positive results with clear graphics	<ul style="list-style-type: none">● No explicit validation of weight comp.● Experiment only along a single axis● No trial of 30 episodes without FMRLC

- Further Work Suggestion:

- Experimental validation of variable admittance control for translation and rotation about many different axes

Conclusion

- Introduced unique way for tuning variable admittance control for simple rotation tasks
- Provides a lot of insightful mathematics for performing variable admittance control and static tool gravity compensation
- The experiment section was lacking without control trials without FMRLC training and without gravity tool compensation validation

Questions

References

- Dimeas, Fotios & Aspragathos, Nikos. (2015). Learning optimal variable admittance control for rotational motion in human-robot co-manipulation. IFAC-PapersOnLine. 48. 10.1016/j.ifacol.2015.12.021.
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